A Case Study in System Dynamics Optimisation

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Abstract

This paper presents the use of optimisation as a tool for policy analysis and design in system dynamics models and presents a demonstration of its use on the 'project model' developed by G. P. Richardson and A. L. Pugh Ill in their book "Introduction to System Dynamics Modelling with DYNAMO". The use of optimisation to design parameters, table functions and new model structure is shown to produce a very significantly improved performance for this model compared to conventional approaches.

INTRODUCTION

The purpose of this paper is to present a case study to demonstrate the merits of using optimisation for the purpose of policy design in system dynamics models.

Treditionelly, system dynemics hes relied very extensively on the use of intuition and experience by system owners and analysts to help design policies for improving system behaviour over time. This situation is now changing and much effort is being expounded in the development of policy design methods. Basically, two schools of thought ere emerging. The first of these concerns the application of control theoretic methods such as eigenvalue analysis, linear control theory, Routh stability criterion, model . control theory and optional control theory. (Sharma (1985), Mohapatra and S harma (1985). These approaches can be powerful but do required a level of assumption and analytical ability out of keeping with the original aims of system dynamics, which was to facilitate the exploration of systems by as wide a range of practitioners as possible. Intensive use of these methods is not anticipated until computer software is developed to improve their ease of application.

390 THE 1986 INTERNATIONAL CONFERENCE OF THE SYSTEM DINAMICS SOCIETY. SEVILLA, OCTOBER, 1986

The second major aproach to policy design which has emerged in recent uears is that of simulation by optimisation (Keloharju (1983), Gustafson and Wiechowski (1986)). This approach also relies fundementally on computer software but is not inhibiting in it's dependence on sophisticated analutical techniques. The software to be described and applied for optimisation in this paper was originally developed in the late 1970's as an appendage to DYSMAP (Dynamic Simulation Model Application Programme) (Cavana and Coule 1982) and known as DYSMOD (Dunamic Simulation Model Optimiser and Developer). This software is currently under further development by Bradford and Salford Universities in the United Kingdom and will be released shortly as a specific version of the redeveloped and restructured DYSMAP2.

The DYSMOD Optimiser

Although the concept of optimisation is not new in system dynamics, the DYSMOD approach to model development and analysis provides a new dimension to sustem dunamics. The software uses a hill climbing routine to heuristically determine the optimum values for any number of model parameters relative to predefined objective functions or performance measures. Essentially, the method assumes a sustem dunamics model as a starting point. However, experience uses might formulate their models somewhat unconventionally to give the software maximum scope to assist with the task of model development.

Optimisation in parameter space is achieved by interleafing simulation and optimisation. One iteration of the procedure consists, firstly, of a DYSMAP simulation run, in which the value of the objective function is recorded, and secondly in a run of the optimiser to choose parameter values which might improve the objective function. Subsequent iterations consist of rerunning DYSMAP to test out the resultant improvement in the objective function under the new parameters and further refinement of them by optimisation. Any one experiment with the software might take a 100 or more iterations. This procedure presents few problems, however, given efficient software and the current downward trend in computer hardware costs.

One of the more basic and but perhaps more trivial uses of such an optimisation technique (which is often wrongly considered as it's only use) is in fitting models to past data. Whilst the method has an important role in the area of validation, it's much more influential role is in parameter and table function policy design and, less obviously, in structural policy design. The latter is achieved by combining alternative policy equations using pseudo parameters to achieve 'mixed' rather than

'pure' policy analysis. Further, by combining real and pseudo parameters in an experiment, parameter and structural policy design can be carrried out simultaneously and in a process which subsumes sensitivity analysis. In conventional sustem dunamics practice these activities must be carried out separately and sequentially and in a very limited way. In optimisation the model structure can be considered as a continuum and the process considered as one of choosing or sunthesising a final model from an infinite number of possible models. comprised of all the parameter and structural permutations offered (a variety set).

in large scale models the policy design process is further facilitated in DYSMOD by the use of a base vector convention similar to those used elsewhere: for example in the simplex algorithms of mathematical programming. That is, only a limited number of parameters are considered 'free' or in the base at any time; but that the candidate parameters for the base can be changed as optimisation proceeds. Other sophistications available, but outside the scope of this writing are the concepts of model simplification (that is, the driving of psuedo perameter variables to zero to eliminate model structure) and optimisation over variable time horizons within the simulation.

Figure 1 gives an overview of the structure of, and interactive imputs to DYSMOD. During optimisation/simulation only the final values of perameters and objective functions are printed. The rerun facility allows the final 'model' to be run conventionally to examine other model variables and their behaviour over time. Subsequently, further optimisation can be undertaken with revised paramters, objective functions, numbers of iterations, etc.

A Case Studu

1. A Specimen Model. Optimisation as a policy design tool is best demonstrated by using a system dynamics model as its starting point. In order to avoid the devotion of time and space here to introducing a new model it was decided to choose a well known model as a candidate for optimisation. The model chosen for this purpose was the excellent 'project model' (Richardson and Pugh (1981)), originally developed to explain the process of applying system dunamics and to demonstrate the power of the method for exploring the merits of alternative system operating poicies. It should be stressed that this choice is not in any way meant to imply criticism of the policy design method used by Richardson. and Pugh. Indeed the opposite is the case and the work here should be seen as a way of extending the analysis provided by these authors.

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The purpose of the 'project model' was to explore the evolution over time of a project involving a set of tasks. The basic version of the model focused on factors affecting project overruns, and subsequent developments dealt with the introduction of more realism into the model (for example disaggregoting the workforce) and in examining the redesign of peremeter and structure! based polices for control of the project. Performance measures of total project time and labour costs were introduced as a basis by which to compare alternative policies.

An influence diagram of the model tailored to this presentetion is given in Figure 2 and a full listing of the model, including additional equations for the purpose of optimisetion, is provided in Appendix I. Figure 2 is somewhat self explanatory and no further discussion of the existing model will be given here. Instead, the optimisation modifications to the model will be described together with some policy experiments and results for comparison with those achieved on the besic model. Comments will elso be made on these results where they provide evidence of the general insights which con be gain from the optimisation procedures.

2. Amendments to the Model. It will be seen from Appendix I that a supplementary set of equations are introduced into the model (lines $98 -$ 111). Since the optimisetion process consists of many simuletion runs, it is firstly very necessery to heve precisely celculeted perforrnance measures rather than to rely on extracting such information from output graphs. AUX1,, AUX4 therefore store for later calculation the exact time of project completion and variables AUXC1 and AUC2 register the total cost from the project. Secondly, it is necessary to define a suitable objective function. In the case of the project model an appopriate measure is the trade off between the cost and the completion time for the project as given by the equation for OBJ1.

It is steted by Richerdson end Pugh that (for such projects of the type described in the model); "whether or not e policy is on improvement depends on how one weighs the edditional cost egeinst the seving in completion time. A system dynemics model does not set or eveluete the criteria for improved system behaviour people make the value judgements." However, in optimisation it is perfectly feasible to explore such judgements in the model. It will be seen that the equation for OBJ1 incorporates a parameter 'WEIGHT to achieve this. Varying WEIGHT between model experiments ellows the strength of the trede-off between cost and time to be investigated. AUX5 in the equation for OBJ1 is included in order to penelise eerly completion end avoid trival results.

 $(Equations 105; 106, 107 and 110 given in Appendix I facilitate global$ sensitivity analysis and are not used in the experiments described here.)

3. Direct Parameter Policy Design. Richardson and Pugh defined some parameters which were used in their parameter based policy design experiments. These are listed in Table 1 (and highlighted on Figure 2) together with the values allocated to them by Richardson and Pugh in their base model run. This table also sets ranges for these variables which were used in the optimisation experiments. The conventional approach of sustem dunamics is to vary these paramters either one a a time or in combination to establish their effect. Examples of the conventional results obtained by Richardson and Pugh for project cost and time are shown in Table 2. Run 1 on table 2 represents the results from the base run of their model and the second line represents the effect of a new parameter set. Lines 3 - 8 in Table 2 give results from the optimisation experiments. In each line the objective function weight was changed and the parameter values given are those chosen by the optimisation software.

Table 1. Parameters Defined for Parameter Policy Design Experiments.

Table 2 Results of Conventional and Optimisation Experiments for Parameter Policy Design.

Some interesting factors emerge from these results. Firstly, the optimiser results indicate that it is possible to reduce both project time emd cost significantly from the base run; and from the position reached by the individual parameter changes suggested by Richardson and Pugh, by manipulating the four basic parameters. Secondly, time and cost do not appear to be sensitive to the value of the weight attached to these factors in the objective function. Thirdly, that the approximate same time and cost can be achieved by many different permutations of the perameters. This result might be considered to contribute to the proof of the view that there is no generally right combination. of paremeters for a model, which is often claimed in conventionel simuletion.

It should also be noted here that WFAT and ASMT are chosen to be small. The former implies that workforce imbalances should be eliminated as quickly as possible and the latter that the workforce should be. assimilated as quickly as possible. This may of course incur additional training costs and highlights the need for this factor to be included in the model. In fact, it is interesting to reflect that such low values of these parameters might never have been tested out in conventional system dynemics policy analysis, since conventional wisdom would heve expected instabilities to have been creeted. Conversely, the results imply thet the scheduled adjustment time (SAT) and the time to percieve progress (TPPROD) need not be low.

Finally, it should be noted that identical results are obtained with weights of 6.7 end 6.8. This results implies thet model beheviour is not necessarily elways a function of policies end that whet is really important in sustem dunamics is the point along each continuous parameter trajectory at which behaviour does change.

4. Table Function Policy Design. As an alternative to changing specific parameters in the model, policy design cen elso be cerried out by varying teble functions. Three of the teble functions suggested by Richardson and Pugh for this purpose are given in Table 3. These are also highlighted in Figure 2. Teble 3 defines each of these functions ond gives the ranges of ·the tables used in the optimisotion experiments. In each case the first boundary given is that used in the base run of the model by Richardson and Pugh.

Run 1 in Table 4 shows an example of the results obtained by Richardson and Pugh from changing TWCWF alone relative to the base model run and setting this at the alternative boundary defined in Table 3. Runs 2, 3 and 4 in Table 4 show the results from optimisation when the previous parameters, plus each table function in turn, are chosen by the software. Run 5 allows a pair of table functions to change together. All optimisetion experiments were carried out a weight value of 0.6.

THE 1986 INTERNATIONAL CONFERENCE OF THE SYSTEM DINAMICS SOCIETY. SEVILLA, OCTOBER, 1986 397

TABLE 3. Table function defined for Policy Design Experiments.

TABLE 4. Results of Conventional and Optimisation Experiments for Table Function Design.

In general the results in Table 4 again show significant improvement in both time and cost for the project relative both to the base run and the Table 2 results. Run 2 suggests en interesting policy a)ternetive which changes loop polarities. That is thet the time to discover rework should be a concave function of the project progress rather than a convex function. This function is chosen to be to close to its lower boundary which suggests that the fester rework is discovered the better for the project. This, in turn, suggests better quality control is needed and indicates, realistically, that the cost of this should be taken into account in the model. In runs 3 and 4 the optimisation also chose the alternative boundaries of TWCWF and TNFSAT for which the same conclusions can be drawn as for run 2. In run 5 the model developed in run 4 for TNFS was taken as a starting point end the other two table functions optimised. The results are the best of this group.

5. Structural Policy Design, Richerdson and Pugh also introduced structural policy design experiments into their model. An overestimation parameter was introduced for this purpose end considerable discussion was presented by these authors es to whether overestimation should be applied to effort perceived remaining on the project or to the indicated workforce. The final choice for locating this parameter was recommended to be in the equation for the effort perceived remaining. In order to investigate this issue using optimisation two overstimation parameters were defined. As will be seen in the appendix OE1 was defined in the equation for effort perceived remeining end OE2 was defined in the equation for the indicated workforce. An experiement was then conducted allowing DE 1 end OE2 to very bet ween 1 end 3 and ell owing ASMT, SAT, WFAT and TPPROD to vary as defined in Table 1. Table 5 shows the results of this experiment with weight values from 0.4 to 0.65 (runs 2-7) together with the Richardson end Pugh result from the bese model with OED inserted in the effort perceived remaining equation at e value of 1.5.

In ell cases of the optimisation results in Teble 5, the project schedule of 40 weeks could be kept, and at a reasonable cost. (This cost could possibly be improved even further by incorporating the table function related policies defined eerlier). The results also shed considerable light on the choice between OE1 and OE2. In the project model OE1 can be considered to represent an overestimation of demand and OE2 an overestimation of supply. When cost considerations ere more important that time time considerations (WEIGHT is small) there is no need to push supply. Therefore, $OE2=1$ and $OE2=1$. When time is more important than cost (WEIGHT is large) there is no need to push demand. Therefore, $OE1 = 1$ end $OE2 \ge 1$. In other words the two overestimation parameters were

never chosen to be effective together but a clear point emerged at which it was preferable to switch from one to the other. This situation is somewhat analogous to the situation of monetary policy in economics and Table 5 gives and answer to the question as to when to switch from 'restrictive monetory policy' to 'expansionist monetory policy' and vice-verse

TABLE 5, Results of Conventional and Optimisation Experiments for Structural Policy Design.

CONCLUSIONS

This paper has presented the rationale for, and a case studu of the merits of, optimisation for policy design in system dynamics models. When implemented through a good computer software interface the procedure is entirely straightforward to perform. The results produced are, as in conventional sustem dunamics, totally explainable in terms of the underluing feedback structure of the model. However, the saving in conputational effort required by the analyst in producing policy insights is enormous. This is not, however, to say that the level of thinking is reduced. Rather this is increased, since considerable skill is necessary in formulating the model so as to provide the computer with the sufficient scope to generate the maximum amount of model exploration.

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THE 1986 INTERNATIONAL CONFERENCE OF THE SYSTEM DINAMICS SOCIETY. SEVILLA. OCTOBER. 1986 401

Appendix 1

 \circ * REVISED PROJECT MODEL NOTE $\mathbf{1}$ \overline{c} **NOTE** REAL PROGRESS з NOTE L CRPRG.K=CRPRG.J+DT*RPRG.JK \overline{A} $\overline{\mathbf{5}}$ N CRPRG=0 R RPRG.KL=APPRG.K*FSAT.K 6 A APPRG.K=WF.K*GPROD.K*ESPGP.K \overline{z} A GPROD. K=NGPROD*EEXPGP.K 8 \mathbf{S} C NGPROD=1 10 A FSAT.K=NFSAT.K*EEXPFS.K*ESPFS.K A NFSAT.K=TABHL(TNFSAT,FCOMP.K,0,1,.2) 11 T TNFSAT = . 5/.55/.63/.75/.9/1 12 13 **NOTE** 14 **NOTE** EFFECTS OF EXPERIENCE AND SCHEDULE PRESSURE 15 **NOTE** A EEXPGP.K=TABHL(TEEXPG,FEXP.K,0,1,.2) -16 TEEXPG=.5/.55/.65/.75/.87/1 17 τ A FEXP.K=EXPWF.K/WF.K 18 A EEXPFS.K=TABHL(TEEXPF,FEXP.K,0,1,.2) ាព 20 T TEEXPF=.5/.6/.7/.8/.9/1 21 A ESPFS.K=TABHL(TESPFS, ICD.K/SCD.K, .9, 1.2, .05) 22 T TESPFS=1.1/1.05/1/.96/.9/.83/.75 A ESPGP.K=TABHL(TESPGP, ICD.K/SCD.K,.9,1.2,.05) 23 24 T TESPGP=.9/.92/1/1.1/1.18/1.23/1.25 25 NOTE 26 **NOTE** UNDISCOVERED REWORK 27 **NOTE** R GURW.KL=APPRG.K*(1-FSAT.K) 28 29 L URW.K=URW.J+DT*(GURW.JK-DURW.JK) 30 N URW=0 51 R DURW.KL=URW.K/TDRW.K A TDRW.K=TABHL(TTDRW,FPCOMP.K,0,1,.2) 32 22 T TTDRW=12/12/12/10/5/.5 34 A CPPRG.K=CRPRG.K+URW.K 35 A FPCOMP.K=CPPRG.K/CPD.K 36 A CPD K=TABHL (TCPD, FCOMP, K, 0, 1, .2) 37 T TCPD=800/830/900/1000/1140/1200 38 A FCOMP.K=CRPRG.K/1200 39 NOTE EFFORT PERCEIVED REMAINING 40 NOTE 41 **NOTE** 42 A EPREM.K=OE1*(CPD.K-ACPRG.K)/PPROD.K 43 C DE1=1 A ACPRG.K=CPPRG.K-AURW.K 44 45 A AURW.K=ADURW.K*ATDRW.K 46 A ADURW.K=SMOOTH(DURW.JK,TADURW) 47 C TADURW=8 48 A ATDRW.K=TABHL(TATDRW,FPCOMP.K,0,1,.2) 45 T TATDRW=8/8/7/5/3/1.5 50 L PPROD.K=PPROD.J+(DT/TPPROD)(IPROD.J-PPROD.J) 51 N PPROD=GPROD 52 A IPROD.K=WTRP.K*RPROD.K+(1-WTRP.K)*NGPROD C TPPROD=6 53 54 A WTRP.K=TABHL(TWTRP,FPCOMP.K,0,1,.2) 55 T TWTRP=0/.1/.25/.5/.9/1 56 A RPROD.K=NGPROD*FSAT.K

57 NOTE 58 NOTE HIRING 59 NOTE GO A WF.K=EXPWF.K+NEWWF.K 61 L EXPWF.K=EXPWF.J+DT*WFAR.JK
62 N EXPWF=EXPWFN 62 N EXPWF=EXPWFN 63 C EXPWFN=2
64 R WFAR.KL= 64 R WFAR.KL=NEWWF.K/ASMT 65 C ASMT=6 66 L NEWWF.K=NEWWF.J+DT*(HR.JK-WFAR.JK)
67 N NEWWF=NEWWFN 87 N NEWWF=NEWWFN
88 C NEWWFN=1 68 C NEWWFN=1 69 R HR.KL=(WFS.K-WF.K)/WFAT
70 C WFAT=3 70 C WFAT=3
71 A WFS.K= 71 A WFS.K=WCWF.K*IWF.K+(1-WCWF.K)*WF.K
72 A WCWF.K=TABHL(TWCWF,TREM.K,0,21,3) 72 A WCWF.K=TABHL(TWCWF,TREM.K,0,21,3)
73 T TWCWF=0/0/0/.1/.3/.7/.9/1 73 T TWCWF=0/0/0/.1/.3/.7/.B/1 74 A IWF.K=OE2*EPREM.K/TREM.K 75 C OE2=1 76 NOTE 77 NOTE SCHEDULING 78 NOTE 79 A TREM.K=SCD.K-TIME.K 80 L SCD.K=SCD.J+DT*NAS.JK
81 N SCD=SCDN 81 N SCD=SCDN
82 C SCDN=40 82 C SCDN=40
83 R NAS.KL= 83 R NAS.KL=(ICD.K-SCD.K)/SAT
84 C SAT=6 84 C SAT=6
85 A TCD K 85 A ICD.K=TIME.K+TPREG.K 86 A TPREG.K=EPREM.K/WFS.K OBJECTIVE FUNCTIONS 88 NOTE 89 NOTE INDICATORS
90 NOTE 80 NOTE 91 L CUMEFF.K=CUMEFF.J+DT*(WF.J*ESPGP.J)
92 N CUMEFF=0 82 N CUMEFF=0
93 A COST.K=C 93 A COST.K=CPMM*CUMEFF.K
94 C CPMM=3000 94 C CPMM=3000 95 NOTE 86 NOTE ******EGUATIONS FOR OPTIMISATION ************** 87 NOTE * 88 A AUX1.K=CLIPCTIME.K,0.25,CRPRG.K,CPD.Kl * 99 A AUX2;K=SAMPLE(AUX1;K,AUX1;K,O)
100 A AUX3;K=CLIP(100,0,25,AUX1;K-AUX2;K,1) * 1.00 A AUX3.K=CLIP(100,0.25,AUX1.K-AUX2.K,1)
101 A AUX4.K=SAMPEE(AUX2.K,AUX3.K,0) * 101 A AUX4.K=SAMPLE(AUX2.K,AUX3.K,O) 102 A AUXC1.K=SAMPLE(COST.K,AUX1.K,O 102 A AUXC1.K=SAMPLE(COST.K,AUX1.K,O)
103 A AUXC2.K=SAMPLE(AUXC1.K,AUX3.K,C 103 A AUXC2.K=SAMPLE(AUXC1.K,AUX3.K.O)
104 A AUX5.K=MAX(40-AUX4.K.O). 104 A AUX5.K•MAXC40-AUX4.K,QJ. * 105 C INIT=Q · * 106 C INCR=0.01
107 A TARG.K=(1 107 A TARG.K=(1+INCR)*INIT
108 A DBJ1.K=WEIGHT*(1E+5)+ 108 A 08J1.K•WEIGHT•C1E+5l•AUX4.K+C1-WEIGHTi*AUXC2.K+ * 109 X (1E+5)*AUX5.K
110 A 0BJ2.K=MAX(AU 110 A OBJ2.K=MAX(AUX4.K-TARG.K,TARG.K-AUX4.K) * * * * *
111 C WEIGHT=0.5 * C WEIGHT=0.5 112 NOTE $\qquad \qquad$ 113 NOTE *****·**********************":******************* **NOTE** 115 NOTE CONTROL STATEMENTS 116 NOTE C DT=0.25 118 C PLTPER=2
119 C PRTPER=4 119 C PRTPER=40
120 C LENGTH=80 120 C LENGTH=80
 121 PRINT $1)$ NF, 121 PRINT 1)WF,SCD,OBJ2/2)CUMEFF,FCOMP,FPCOMP/3)COST,OBJ1,
122 X AUXC1/4)AUXC2,AUX1,AUX2/5)AUX3,AUX4,AUX5 122 X AUXC1/4)AUXC2,AUX1,AUX2/5)AUX3,AUX4,AUX5
123 PLOT WF=W(0,80)/SCD=S(30,70)/CPPRG=P,CRPRB PLOT WF=W(0,80)/SCD=S(30,70)/CPPRG=P.CRPRG=R.URW=U(0,1200)/ 124 *X PPROD=**(.6,1)
125 RUN 125 RUN 126' +